



Thomas Zemb

lecture n°9:

*Handling liquid contact in practice:
column, centrifuge and pertraction*

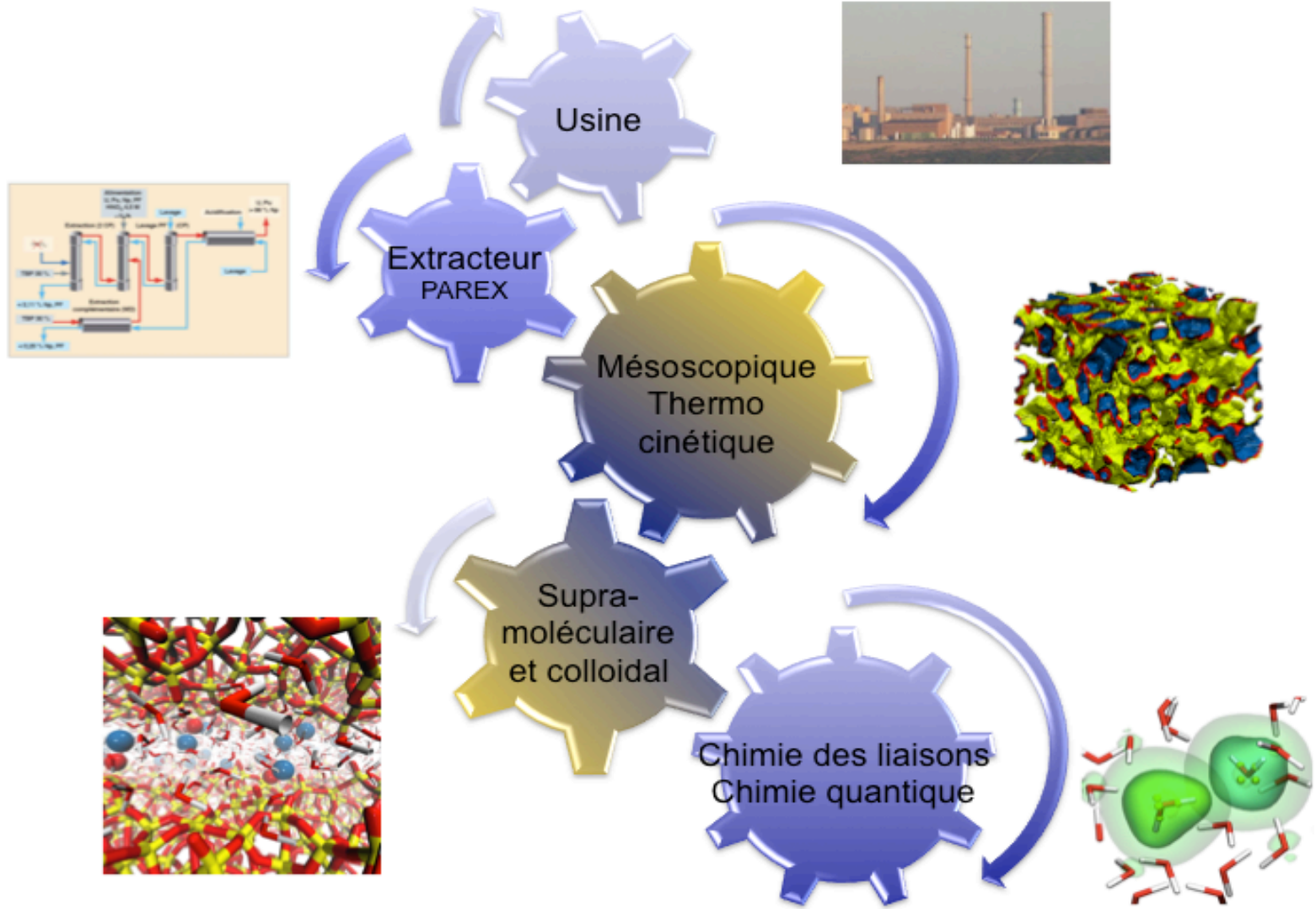
Jean Duhamet



2014-2015



An intrinsic multi-scale approach :





- **Basic concepts at macroscopic scale:**

0/ Settling tanks

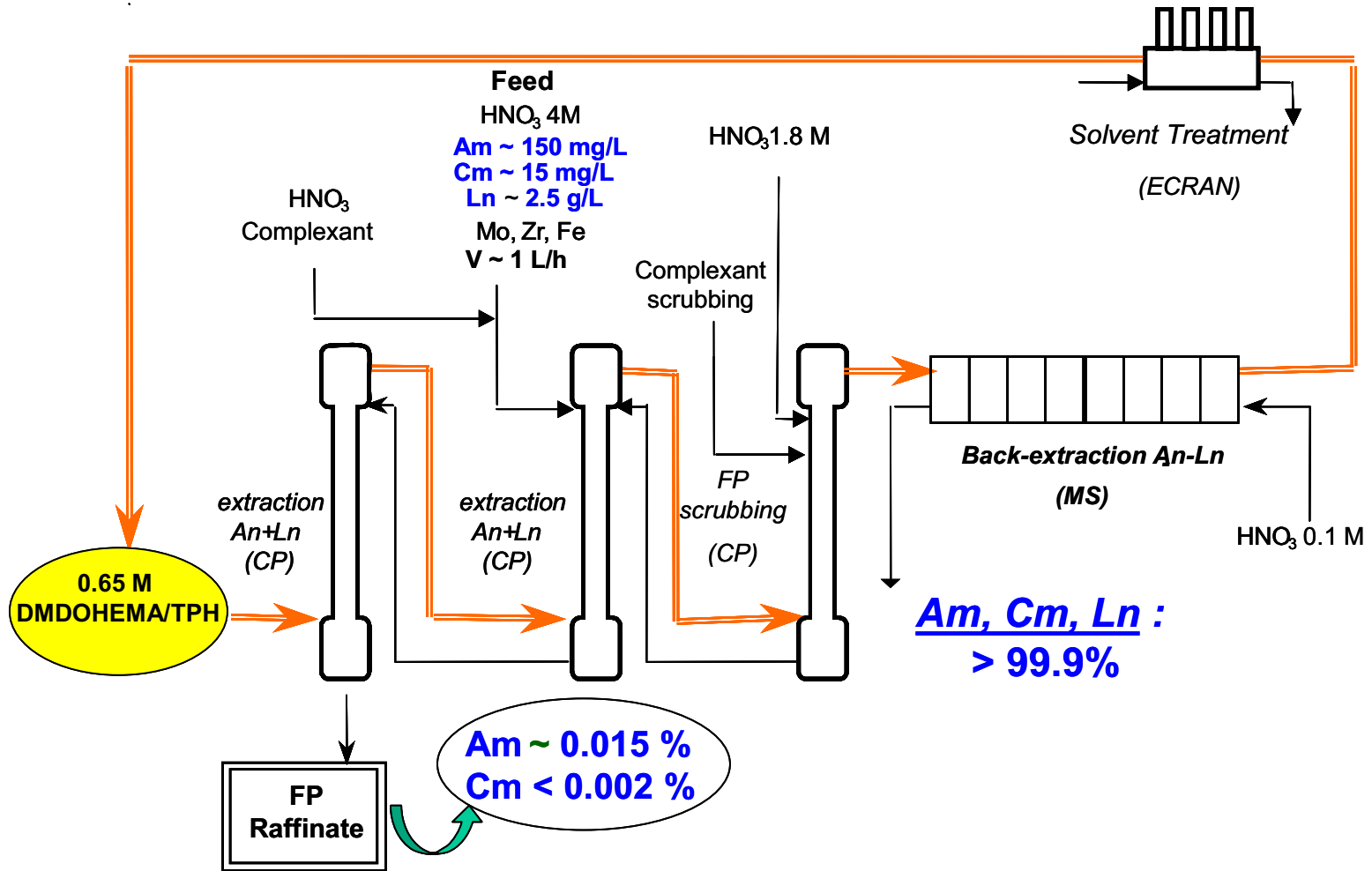
1/ Pulsed columns

2/ Centrifuges

3/ Pertraction



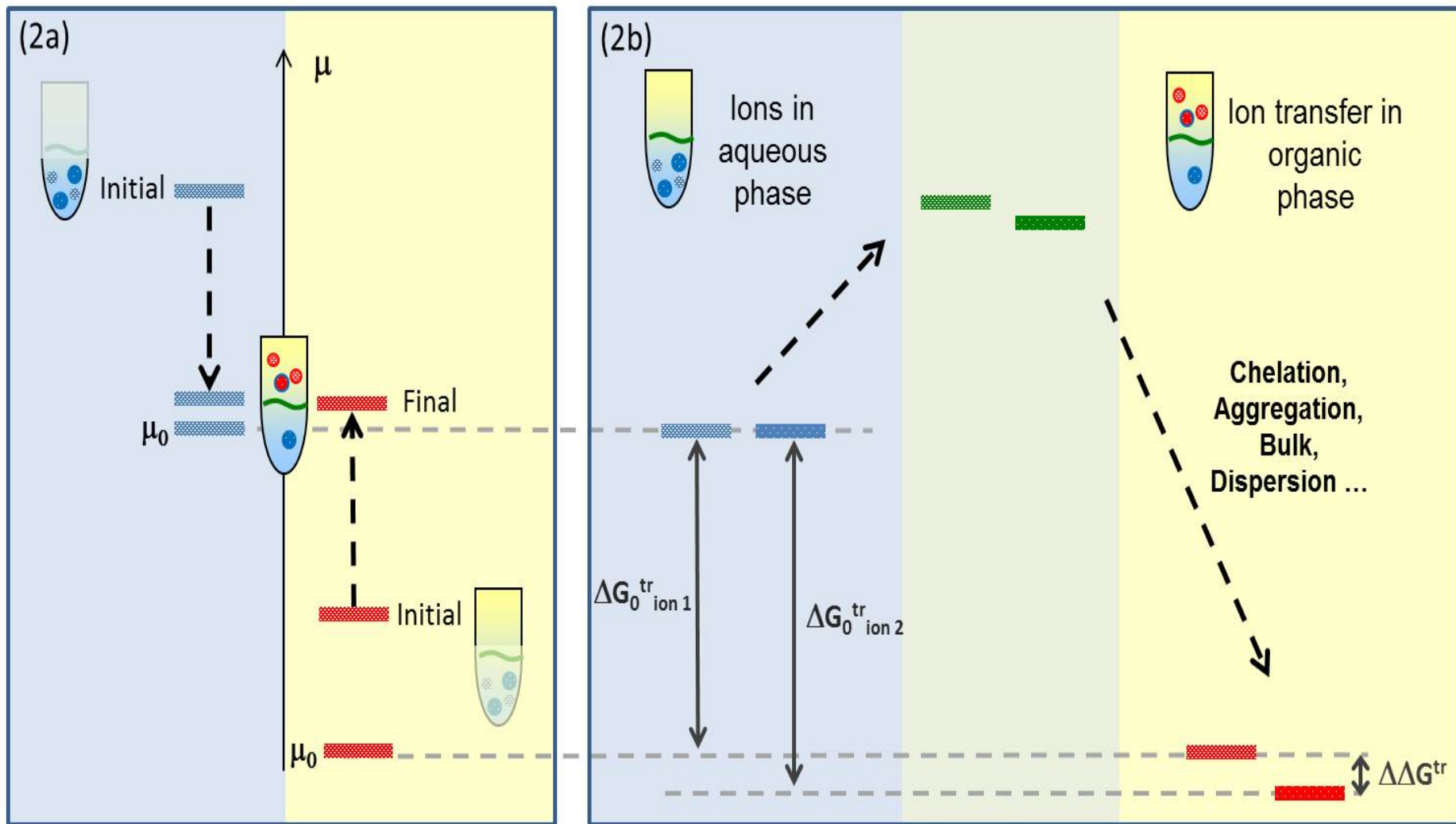
The coupled cascades and solvent treatment



P. Baron et al., , Global 2007



The transfer between phases at meso-scale (next lecture)





Technologies of liquid-liquid extraction

All devices combine:

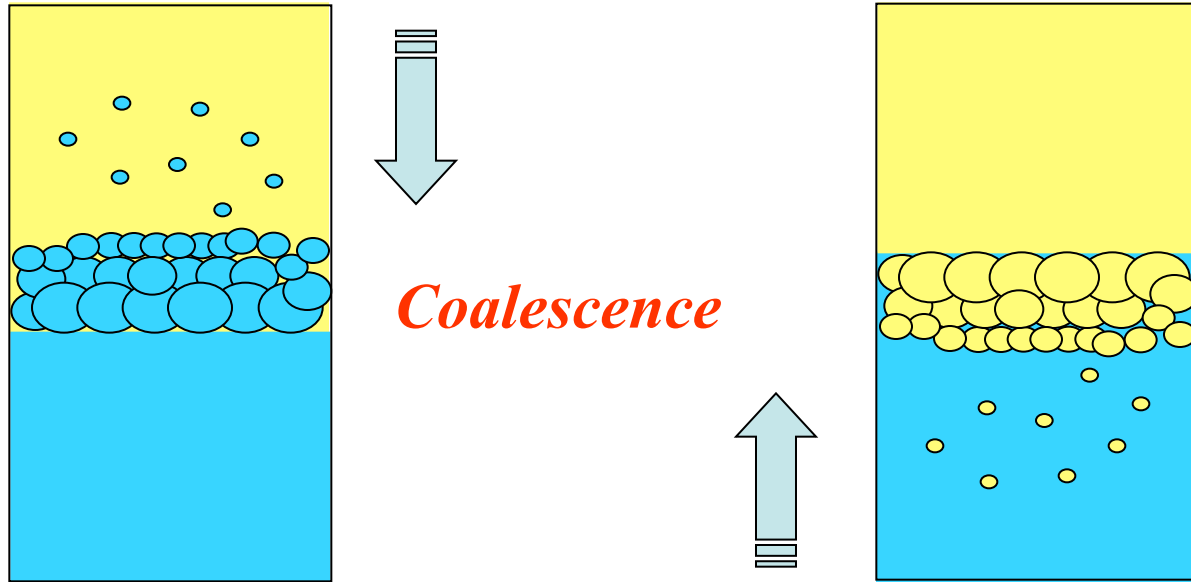
- Some part devoted to mixing/contact
- Some part devoted to phase separation: desemulsification, driven by surface tension effects

Continuous operation at optimized size:

- Large area of contact : **expressed as Σ in (m²/g)**
- Separation of the emulsion (most frequent case microemulsion/brine):

Depends on dynamic and static surface tension, viscosity and density difference that can be tuned by use of formulated solvents (see lecture by Werner Kunz)

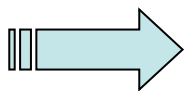
When miroemulsions are formed, and concentration of aggregates becomes too high, the thermodynamcis goes from two phase to three phase « mayonnaise », (see next lecture)



Coalescence

Émulsion FOC
Fonctionnement
Organique Continu

Émulsion FAC
Fonctionnement
Aqueux Continu



Transport via sedimentation or creaming



(Average) « Sauter » Diameter

$$d_s = d_{32} = \frac{\sum_i n_i d_i^3}{\sum_i n_i d_i^2}$$

Volume fraction :

$$\phi = \frac{V_{dispersed}}{V_{Total}}$$

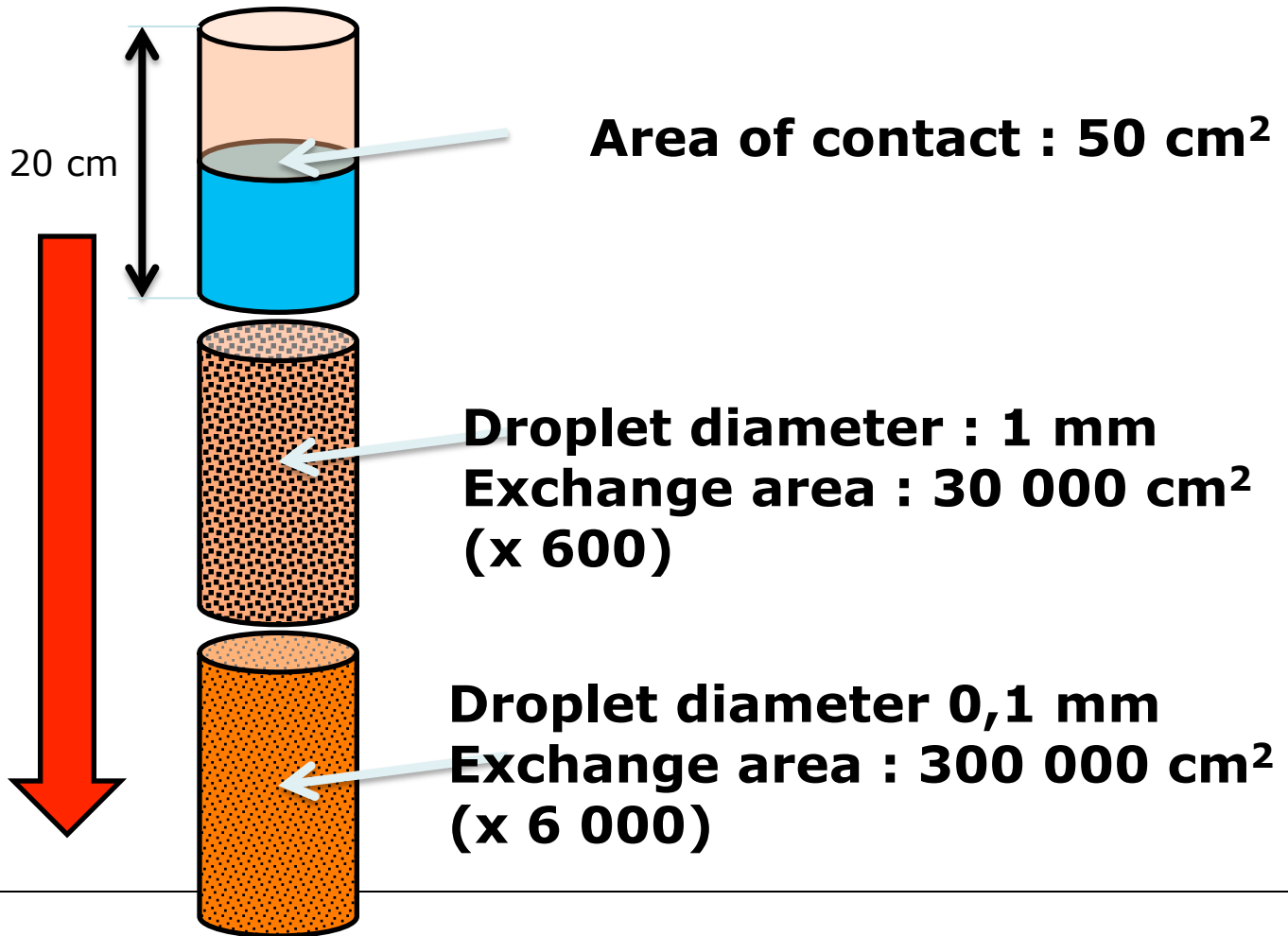
Specific area :

$$\Sigma = \frac{6\phi}{d_{32}}$$



Order of magnitude of area of contact

Numerical Example : 1 liter, with $\phi_0 = 50\%$



Increasing
Shearing
Stress
(Pa)



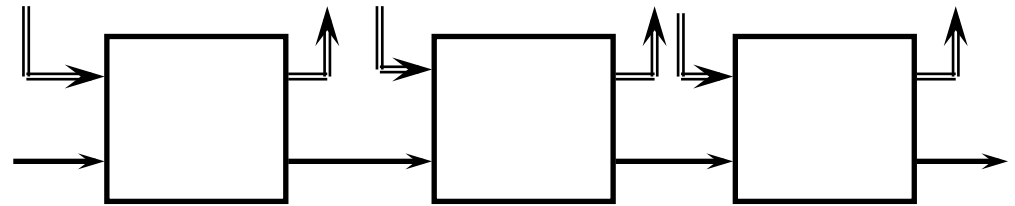
Industrial implementation

- (1) High yield
 - Continuous operation
- (2) High performance
 - Coupling devices
 - In cascades
- (3) Counter-current implementation

Not efficient



Poorly efficient

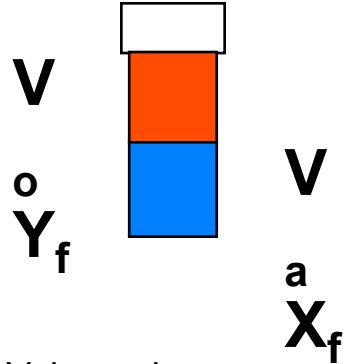


Counter-current :





Étape 3 Décantation des phases



V_A : Vol. aq phase
 V_o : Vol. org phase
 X_f : final C aq phase
 Y_f : final C org phase
 X_i : Ini Conc aq phase

Mass balance

$$V_a \cdot X_i = V_a \cdot X_f + V_o \cdot Y_f$$

Distribution coeff.

$$Y_f = D \cdot X_f$$

Extraction eff:

$$E = \frac{V_o}{V_a} \cdot D$$

Performance d'extraction

One « stage » of extraction

$$\frac{X_i}{X_f} = 1 + E$$

N stage in counter-current configuration (Kremser)

$$\frac{X_i}{X_f} = \frac{E^{N+1} - 1}{E - 1}$$

... interest of high values of E per stage
(typically ten)

... if E too high: desextraction impossible



High stirring stress

Fine emulsion : high Σ



Temperature elevation ?

Micelle existence ?



Visco-elastic effect ?

Solvent Flash point

Low stirring stress

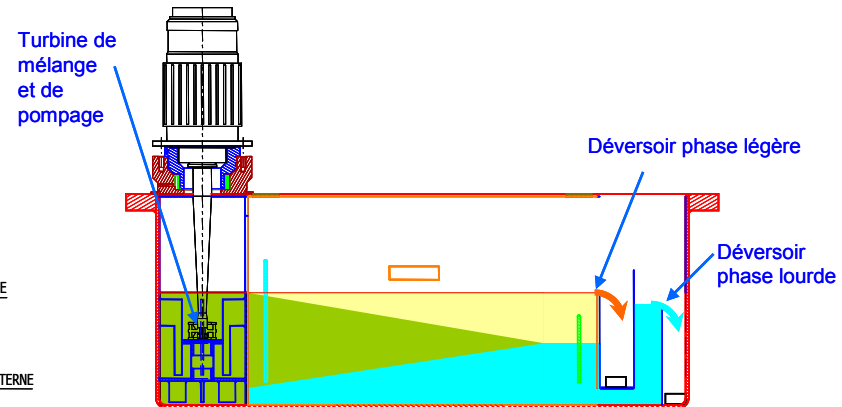
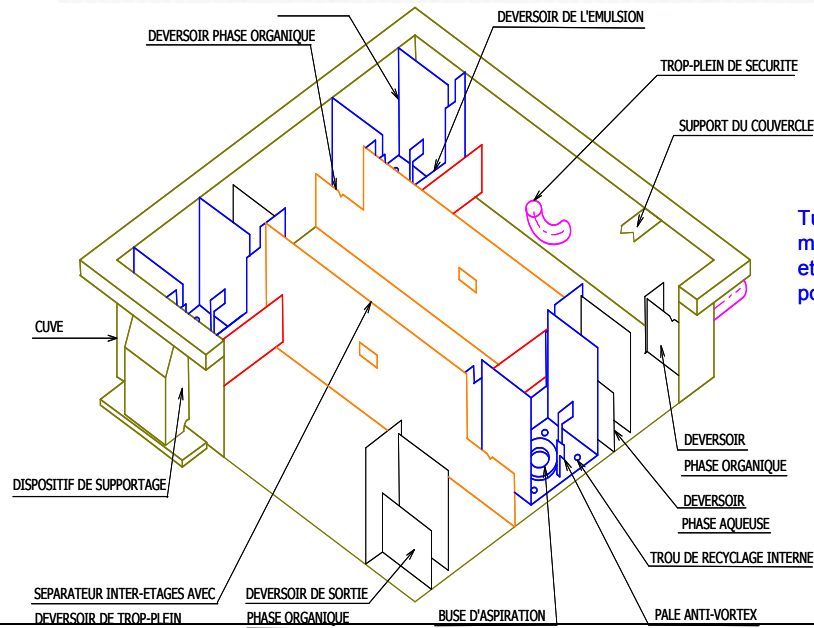
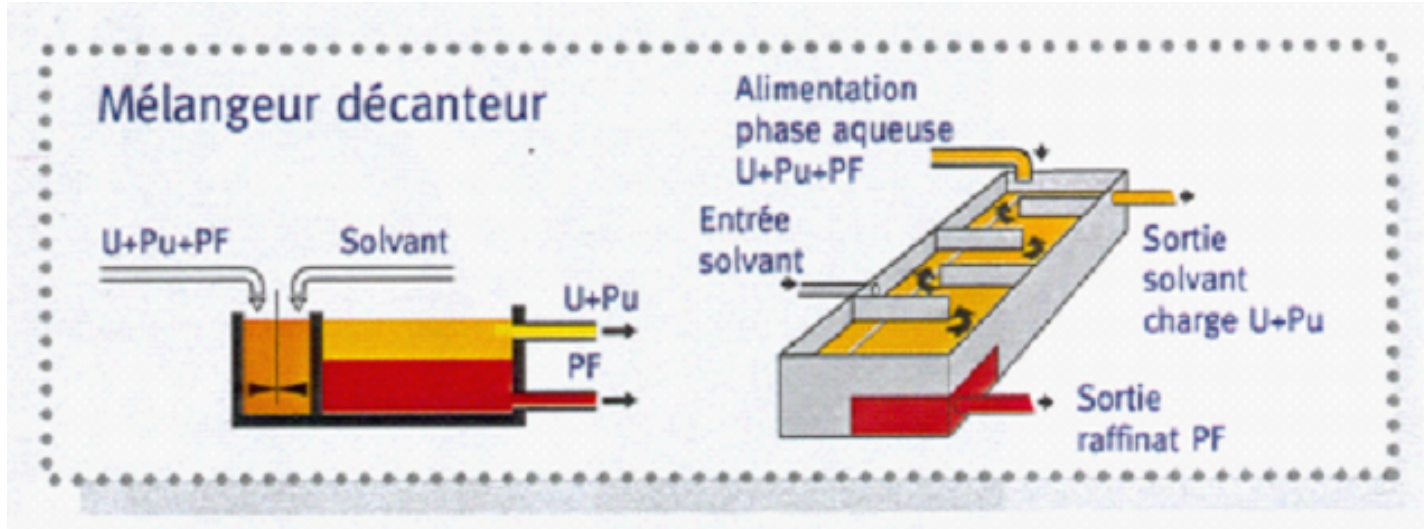
Easy separation between
coarse emulsion droplets

Low yield in feeding/
extracting fluids

Efficiency of
hydrodynamic power



Mixers -settlers in reality



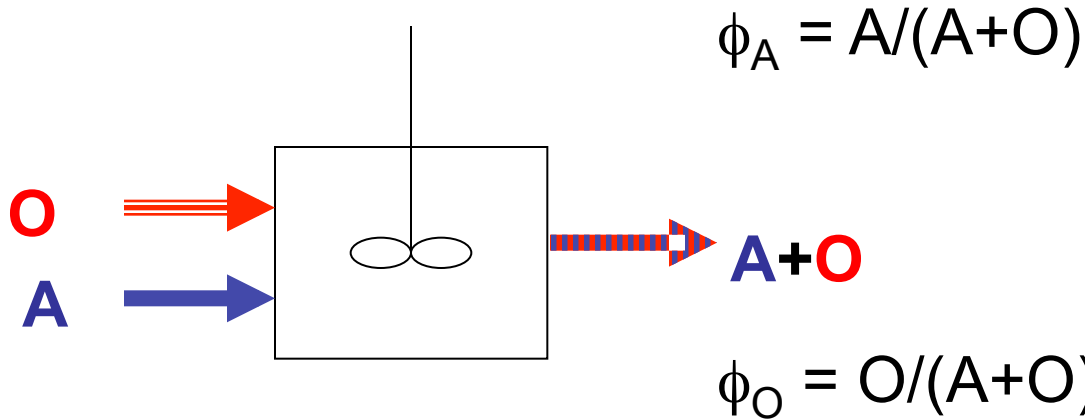


An example at « La Hague »



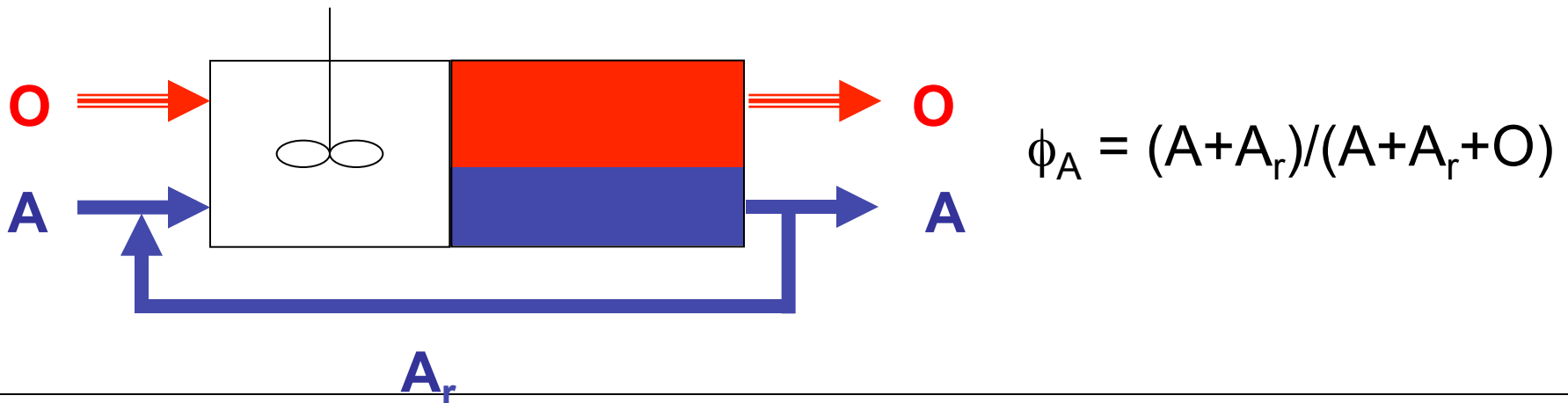


Improving yield of a single stage: partial reinjection



$A \ll O \rightarrow \phi_A \ll 1 \rightarrow$ small Σ

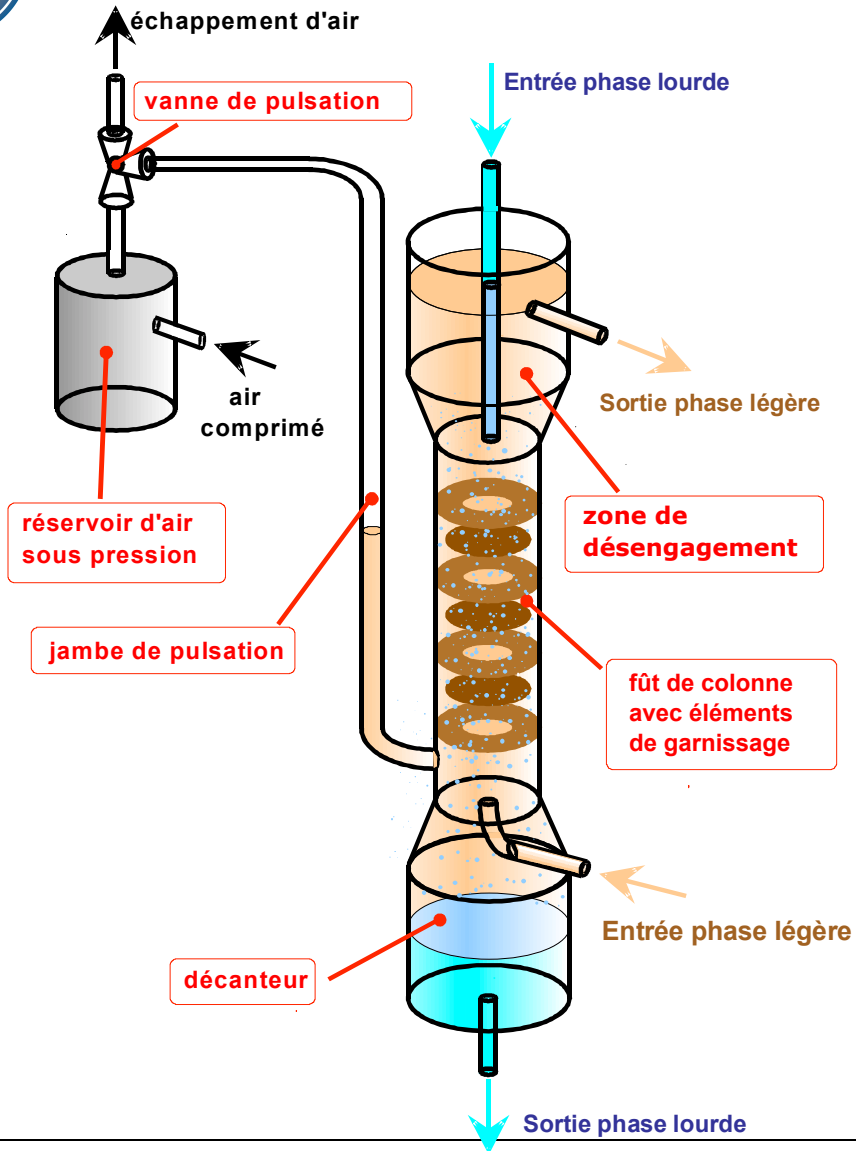
Trick > increase ϕ_A by partial reinjection of aqueous phase



Same trick with organic phase if $O \ll A$

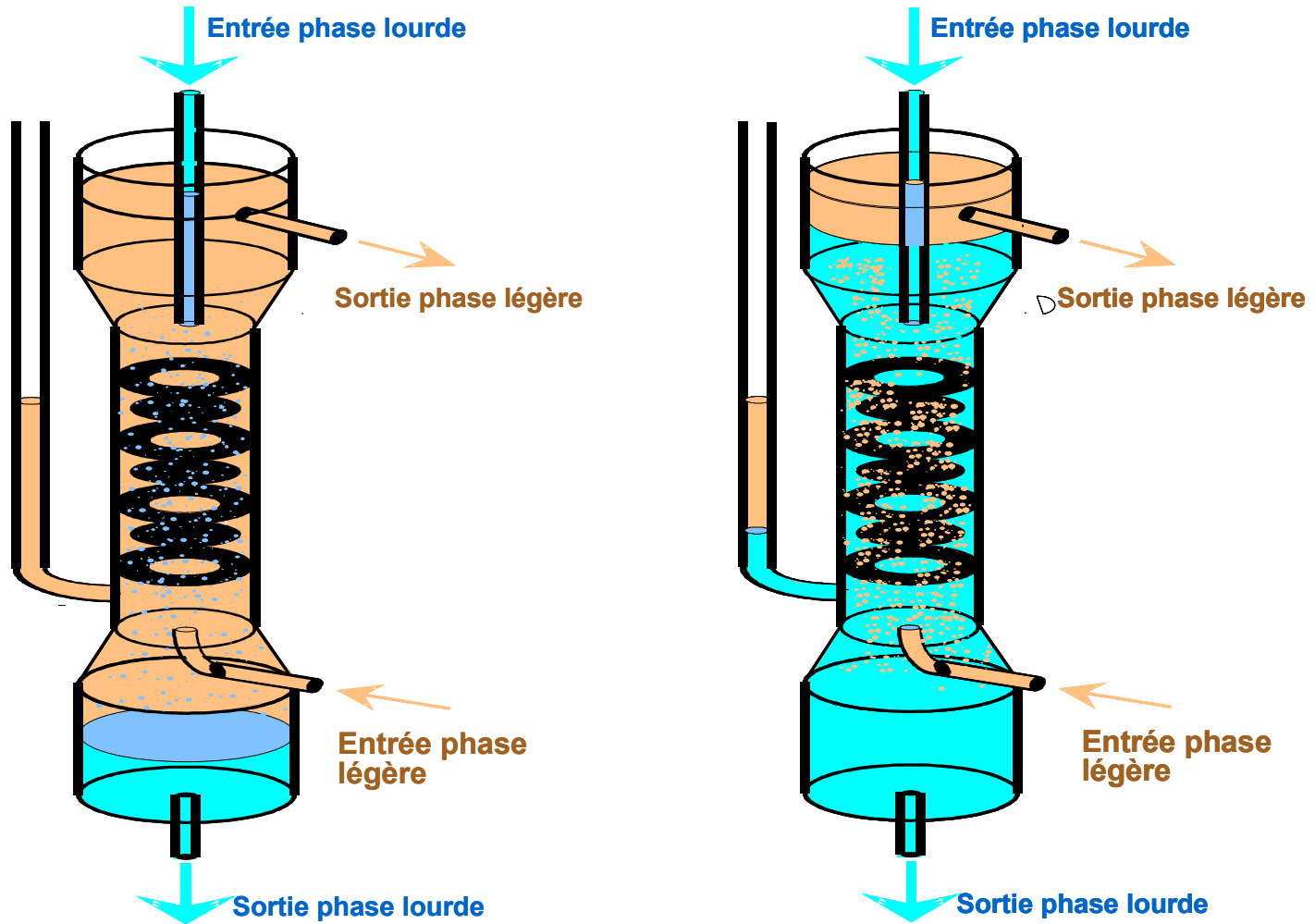


1- pulsed columns





Pulsed columns : o/W or w/o exchange zone





Emulsions filmed in a real column

Registering : 1000
frames/s

View à 25 frames/s

Pulsed columns 15
mm diameter

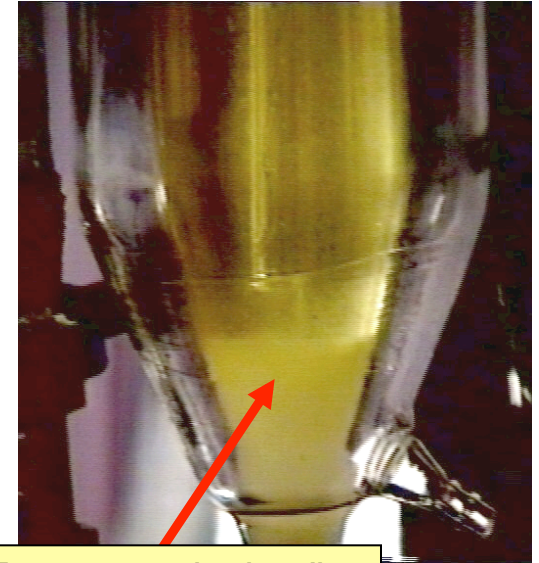




Useful quantities: order of magnitude

- Density of the two coexisting phases
- Viscosity and viscosity ratio
- Interfacial tension (at rest)

Engorgement d'une colonne pulsée



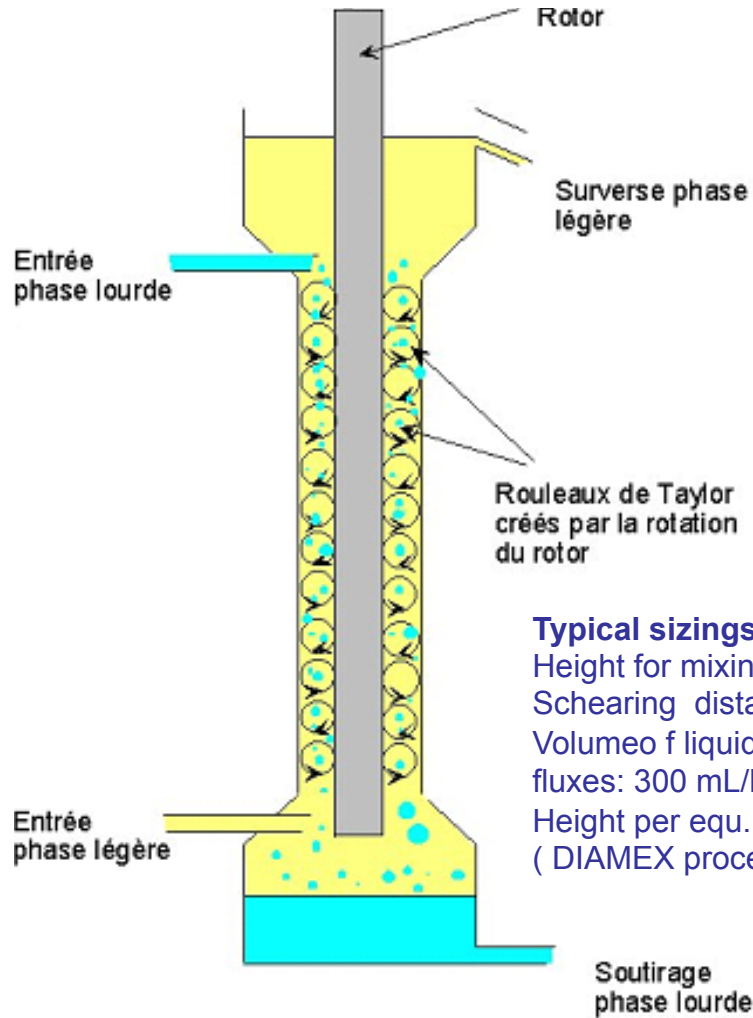
Excess non coalescing oil droplets....

Système de phases	Densité solvant		Viscosité solvant (mPa.s)		Tension interfaciale à 25 °C (mN.m ⁻¹)
	20°C	25°C	20°C	25°C	
TBP 30%-TPH HNO ₃ 2,4 M		0,8459		1,85	10,4
DMDOHEMA 0,65M HNO ₃ 3 M	0,8354	0,8316	6,63	5,57	7,07
DMDOHEMA 0,5M-HDEHP 0,3 M HNO ₃ 3 M	0,8415	0,8378	6,20	5,25	8,21



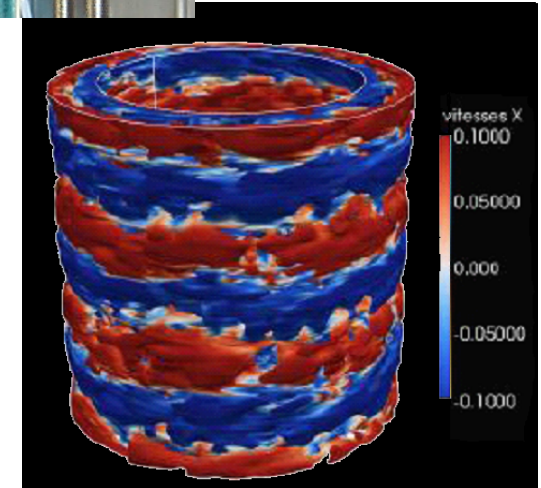
2- Couette cells as separator

Working scheme



Typical sizings

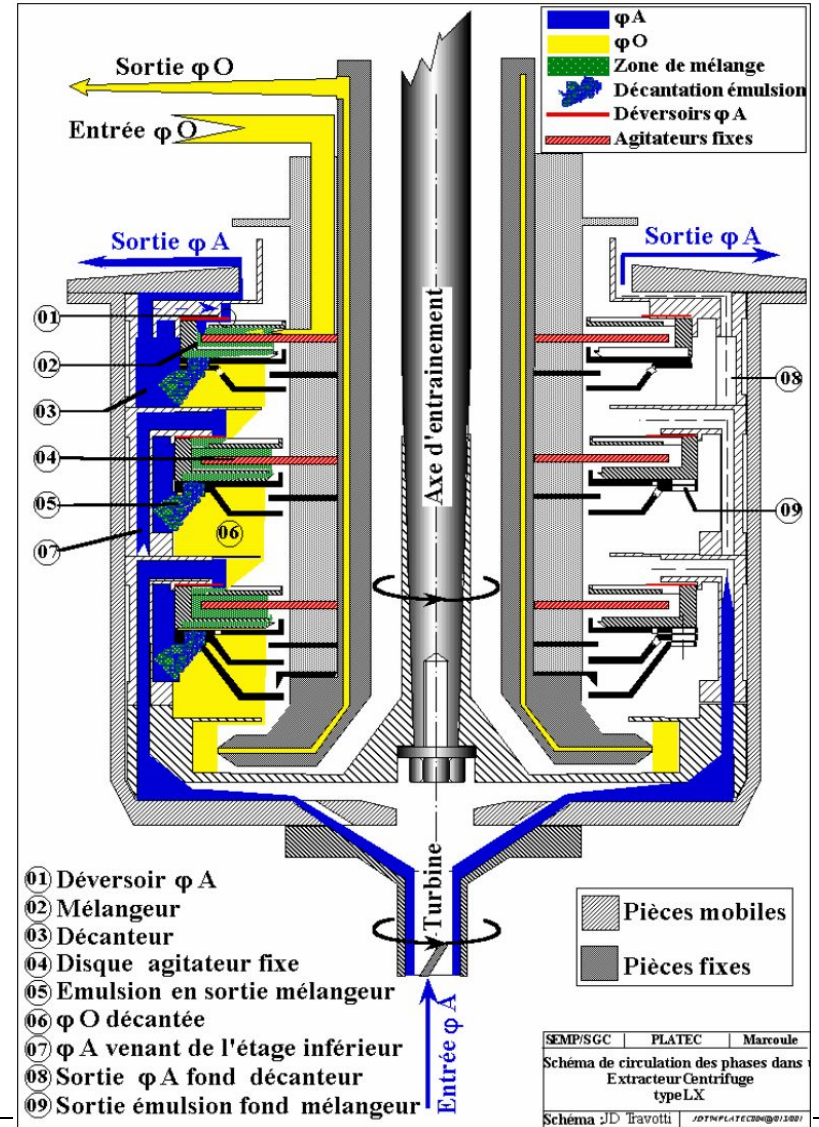
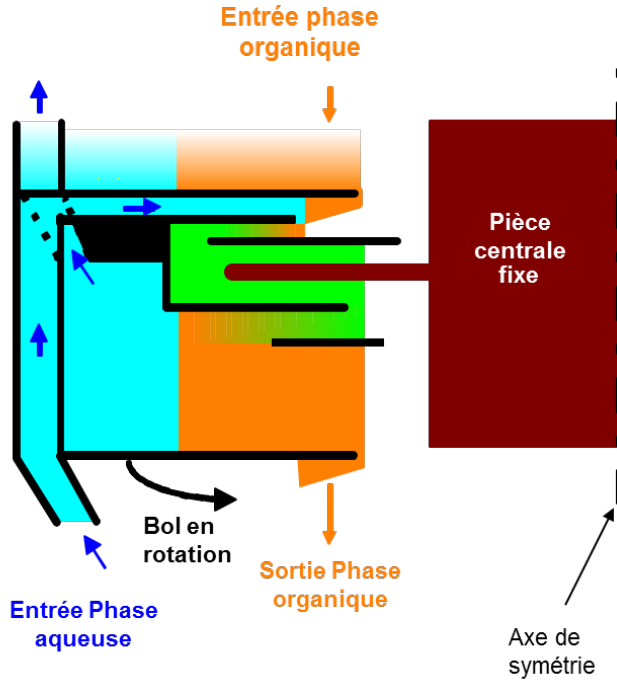
Height for mixing: 50 à 75 cm
Shearing distance: 1,5 mm
Volume of liquid: 80 à 100 mL
fluxes: 300 mL/h (A+O)
Height per equ. stage : 5 cm
(DIAMEX process)



Equivalent to a pulsed column ten times higher



Multi-stage industrial Couette extractor





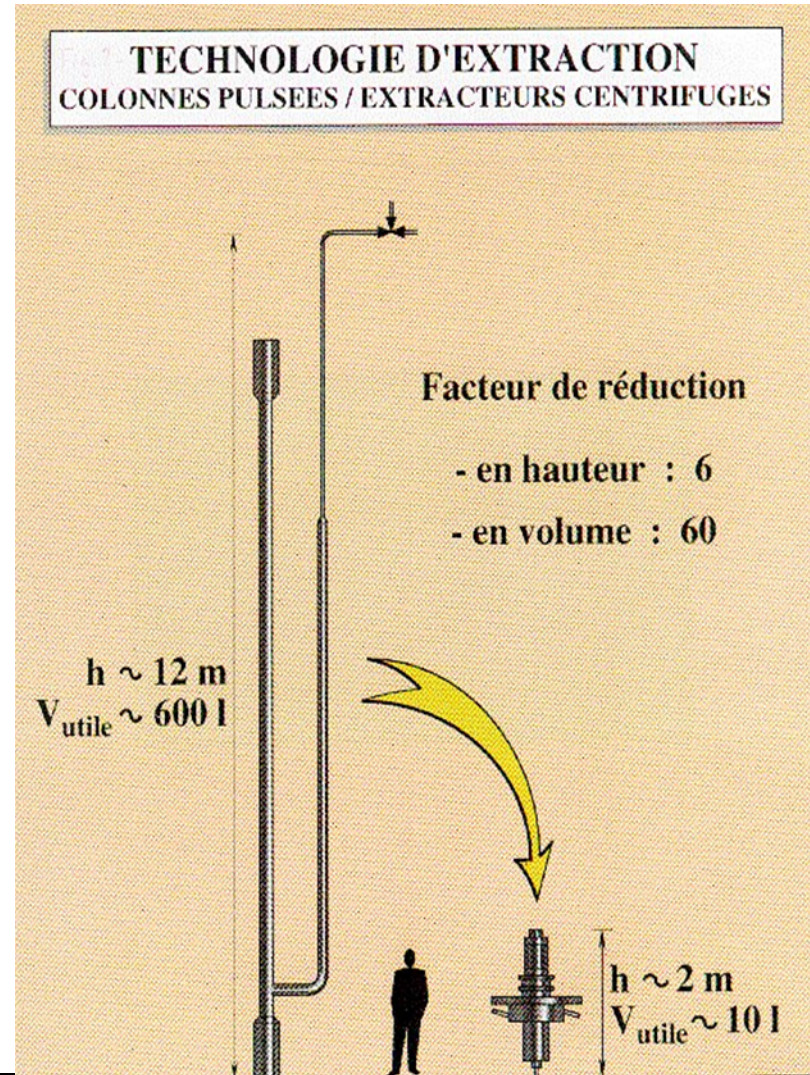
Comparison with pulsed columns

positive

- Compacity
- Limitation of solvent radiolysis
- Low dosis: less fluid present
- Quick equilibration time

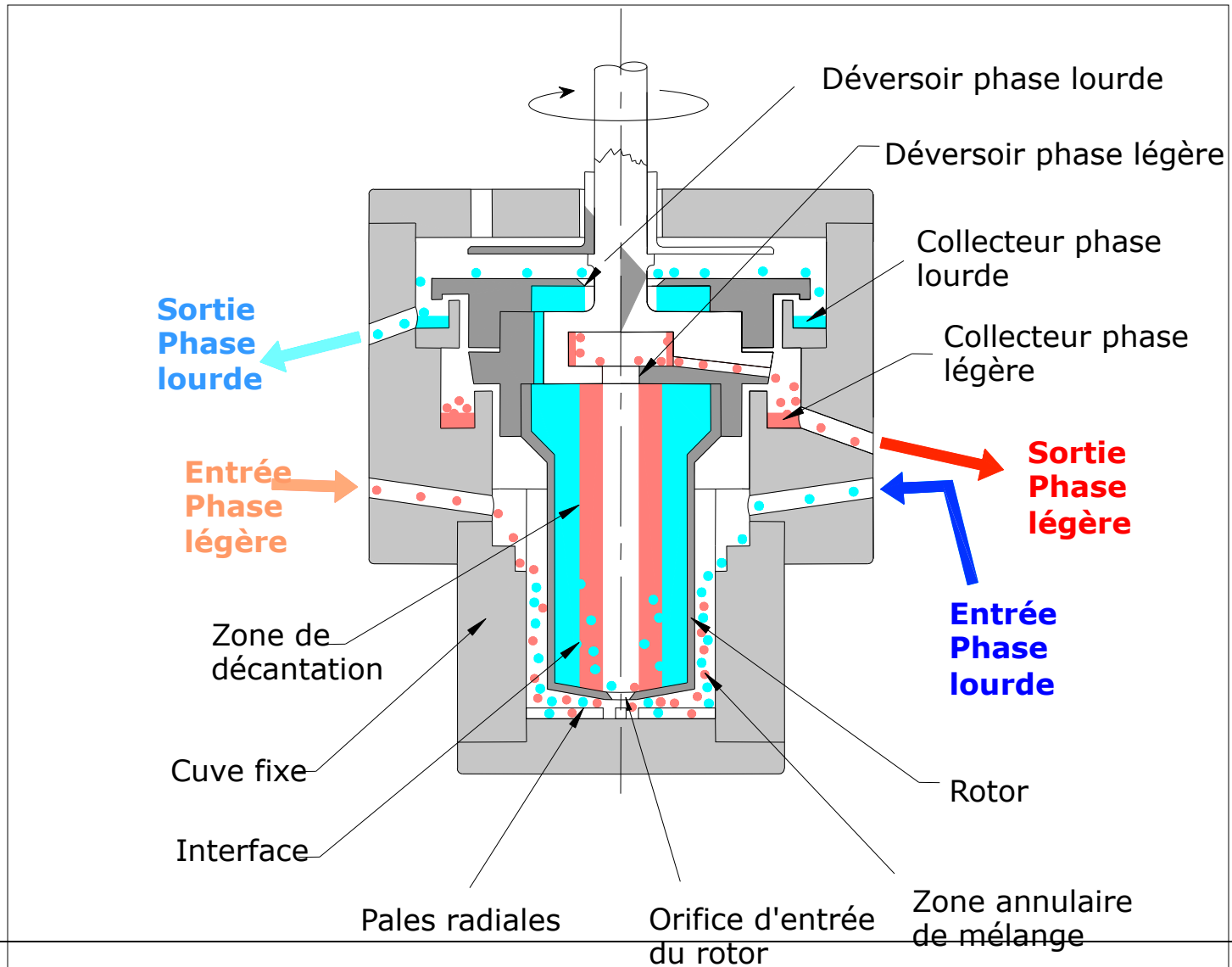
Negative

- O (and w) phase heating
- Fast evolution off spec. working
- Intolerance towards presence of particles
- Maintenance and emptying and refilling problems





Centrifuge extractor designed for La Hague plant



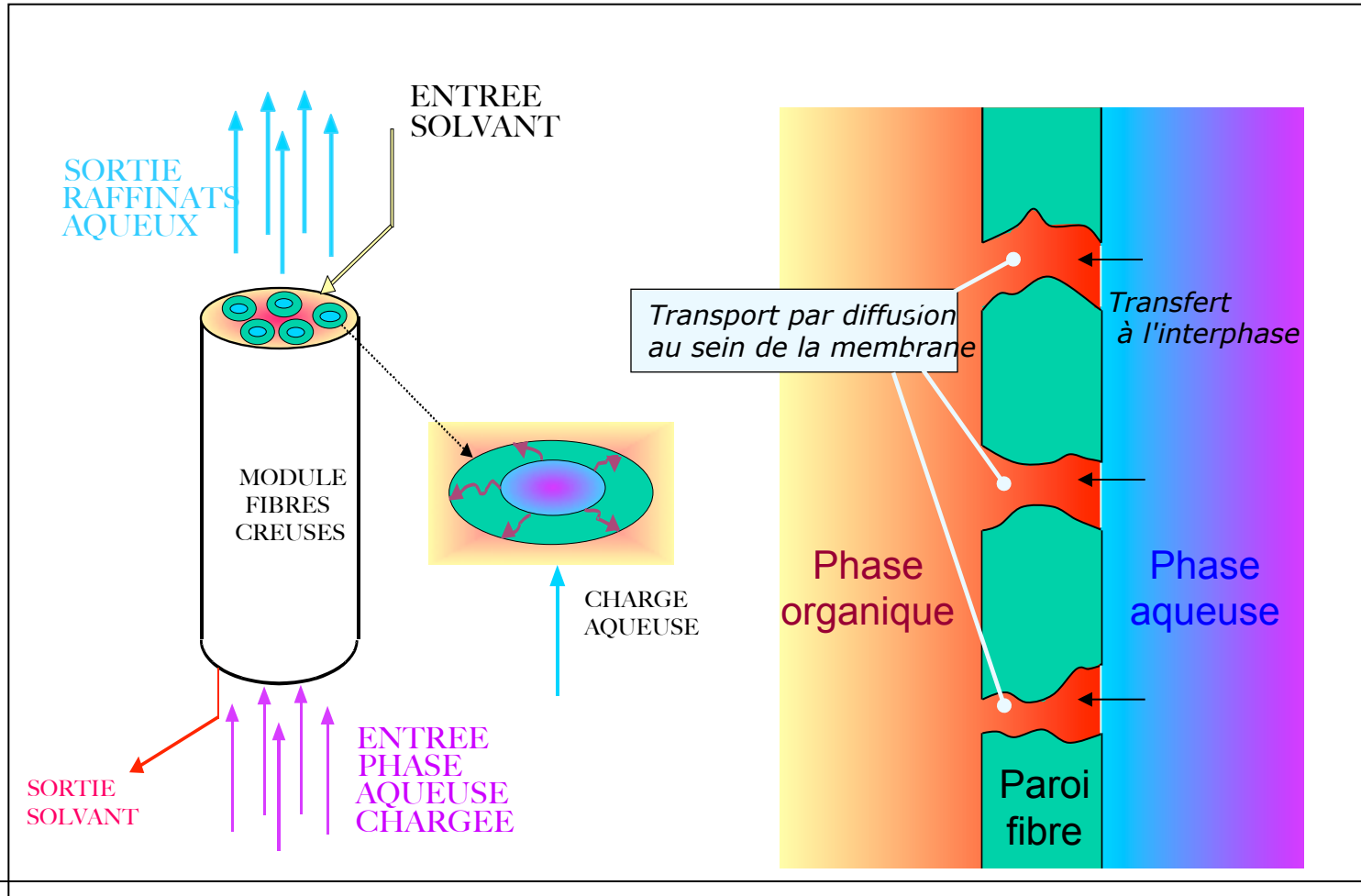


Comparison Mixer/settler, Centrifuge, pulsed column

Device	Mixing time	Separation time	Droplet Diameter	Specific area
Mixer/settler	~ 1 mn	~ 10 mn	~ 0,2 mm	15 000 m ² .m ⁻³
Centrifuge Extracto rLX Robatel	~ 1 s	~ 10 s	~ 0,05 mm	60 000 m ² .m ⁻³
Colonne Pulsée	continuous Phase 40 mn	dispersed phase 10 mn	~ 1 à 2 mm	400 à 900 m ² .m ⁻³
Extracteur Centrifuge laboratoire	1 s à 1 mn	3 s à 3 mn	~ 0,1 mm	30 000 m ² .m ⁻³



A new combined method : pertraction...





Porous fibre extraction :

- Ideal for
 - spontaneously emulsifying systems (low interfacial tension)
 - Solvents of high viscosity
 - No influence of density difference
- Possibilité to use solvent-free systems (or extractant-free systems)
- Simple to operate
- Up-scaling easy

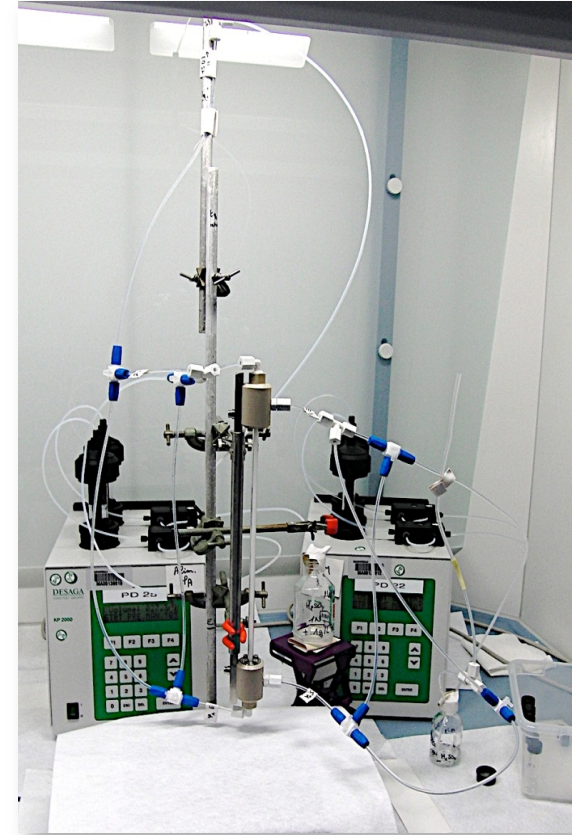
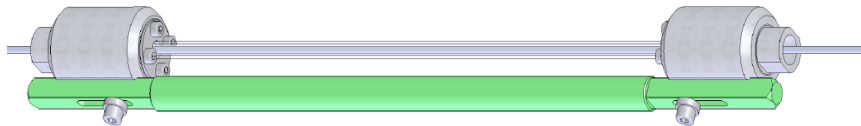


Example using polypropylene fibre

Characteristics

Property		Unit
DiamInternal diameter	1,8	mm
Thickness	400	nm
Length	23	cm
Porosity	75-80	%
Pore diameter	200	nm
Calender diameter	4,5	mm
Area of contact	$1,3 \times 10^{-3}$	m^2

Typical fluxes treated : 1 à 10 mL.h⁻¹





Industrial scale pertraction

Exchange area: 220 m²

Liquid volume *inside* fibers : 21,7 L

Liquid volume *outside* fibers : 33,5 L

Typically 100 000 fibres with 300 µm diameter

